

Optimization of the Heat Bonding Process for Pacemaker Leads: Conceptual Design and Finite Element Analysis

Wilyim Rodríguez Vargas
Master of Engineering in Mechanical Engineering
Advisor: Hugo M. Peláez Carpio, Ph.D.
Polytechnic University of Puerto Rico
Graduate Project EXPO, May 2025

Abstract — This project aims to optimize the heat bonding process used in the manufacturing of pacemakers and leads to bradycardia treatment by redesigning the thermal assembly to improve temperature uniformity, process efficiency, and structural alignment. The original system, which used a dual-stage heating process and an INVAR 36 [1] bar with copper inserts, exhibited significant thermal gradients and misalignment due to thermal expansion. To address this, a new design was developed incorporating Celazole [2] thermal insulators. Finite Element Analysis (FEA) [3] was performed to evaluate thermal behavior. The updated thermal architecture significantly improved temperature consistency across all bonding zones, with improved control and efficiency.

Keywords — Celazole, FEA (Finite Element Analysis), INVAR, Thermal Control.

INTRODUCTION

Cardiac pacemakers are life-sustaining devices used to regulate heart rhythms in patients with bradycardia. At the core of these systems are pacemaker leads, which serve as the electrical conduit between the device and the cardiac tissue. The quality and integrity of the lead assembly, particularly the bond between the polyurethane tube and the platinum-iridium anode, are essential for long-term performance and patient safety. Currently, the manufacturing process for these components relies on a dual-stage thermal bonding technique using an INVAR 36 bar with copper inserts. However, thermal expansion and uneven heating cause alignment issues and bonding inconsistencies.

To resolve these challenges, this project proposes a redesigned thermal assembly using

Celazole insulation and applies Finite Element Analysis (FEA) to optimize thermal behavior and bonding performance.

THEORY

To understand and improve the heat bonding process for pacemaker leads, it is essential to analyze the fundamental physical principles that govern thermal behavior in multi-material systems. This section provides the theoretical background necessary to support the design decisions and simulation approaches applied in this project. Key concepts such as heat conduction, material properties, and thermal expansion are examined in detail to inform the redesign process.

Heat Transfer by Conduction

The thermal bonding process primarily relies on heat conduction [4], governed by Fourier's law, where:

$$q = -k\nabla T \quad (1)$$

- q : heat flux (W/m²)
- k : thermal conductivity (W/m·K)
- ∇T : temperature gradient (K/m)

Effective bonding of polyurethane to Tecothane components requires controlled application of heat to avoid degradation. To ensure uniform bonding without exceeding the degradation point of the polymer, it is crucial to model how heat diffuses across the multilayer assembly. The steady-state heat conduction equation helps evaluate thermal gradients, while transient analysis determines how quickly a stable temperature can be achieved during each bonding cycle.

Thermal Properties of Materials

Copper's high thermal conductivity (~205 W/m·K) facilitates rapid heat transfer but increases the risk of undesired lateral heat flow. INVAR, with its low coefficient of thermal expansion (~ 1.3×10^{-6} /°C), offers dimensional stability even under high-temperature gradients. Celazole (PBI), with a much lower thermal conductivity (~0.4 W/m·K), acts as an effective thermal insulator, isolating the heat-affected zone and protecting adjacent regions from thermal degradation.

Understanding thermal diffusivity is vital in predicting how fast temperature changes propagate through each material. This allows engineers to simulate and tailor heat cycles to maintain safe and effective processing windows.

Material Bonding and Stability

Bonding between the polyurethane (PU) sleeve and the platinum-iridium component occurs through thermal crosslinking, a process initiated once the material reaches its transition temperature. This temperature must remain below the polymer's degradation threshold (~250°C or 482°F). The use of heat shrink sleeves in the pre-heat phase enhances mechanical fit, while the final heat ensures chemical fusion and long-term structural integrity.

Thermal Expansion

Differences in expansion coefficients among materials can lead to mechanical stress and misalignment. This behavior is described by:

$$\Delta L = \alpha L_0 \Delta T \quad (2)$$

Where:

- ΔL : change in length
- α : coefficient of thermal expansion
- L_0 : original length
- ΔT : temperature change

By selecting materials with compatible expansion characteristics or by isolating them using thermal barriers like Celazole, these distortions can be minimized.

FEA for Heat Analysis

Finite Element Analysis (FEA) provides numerical solutions to complex heat transfer phenomena in multi-material systems. The general transient heat conduction equation is where:

$$\rho C_p \frac{\partial T}{\partial t} = \nabla \cdot (k \nabla T) + Q \quad (3)$$

- ρ : material density
- C_p : specific heat
- T : temperature
- Q : internal heat generation rate

By applying FEA to the bonding assembly, it is possible to predict internal temperature profiles under various heating cycles. The model can simulate conduction through copper inserts, evaluate thermal isolation performance by Celazole, and determine stabilization times. These insights support design refinements that ensure bond consistency and reduce thermal distortion.

METHODOLOGY

The methodology involves a multi-phase approach: literature review, conceptual design, and simulation using Finite Element Analysis (FEA). Initial efforts focused on identifying key limitations in the existing bonding process, such as non-uniform heat distribution and mechanical misalignment. A redesigned bonding module was developed using Celazole insulation between copper inserts and the INVAR bar to improve thermal control. 3D CAD models were created to visualize and refine the mechanical layout. FEA simulations were conducted in SolidWorks [5] to analyze both transient and steady-state thermal performance. Simulation data was used to optimize material selection, heat application timing, and geometric design. The updated system was then prototyped, integrated with existing automation and PID [6] thermal control systems, and validated under operational conditions.

PROTOTYPE VALIDATION

Following simulation and redesign, a functional prototype of the new heat bonding system was built and integrated into the production line. The Celazole-based thermal insulation effectively reduced unwanted heat propagation and improved the spatial precision of copper insert alignment. Operator feedback indicated significantly improved ease of installation and alignment accuracy. The new modular insert mounting system also allowed for easier maintenance and part replacement without altering the machine structure. Importantly, the PID thermal control system and machine vision interface continued functioning without modification, ensuring consistent automation performance. These results confirm that the system is robust not only in simulation but also in real-world operation, with the potential to scale into larger manufacturing environments.

RESULTS AND DISCUSSION

Simulation results indicated that the redesigned thermal bonding system achieved significantly improved thermal uniformity and faster stabilization. In the original configuration, copper insert temperatures varied by more than 60°F during the transient phase, as shown in Figure 1. After redesigning, the variation narrowed to less than 5°F, ranging from 455.7°F to 460.6°F (see Figure 2). Additionally, the INVAR 36 bar's maximum temperature dropped from 340.6°F to 119.9°F, as shown in Figures 3 and 4, respectively. As depicted in Figures 5 and 6, the time to reach steady state decreased from 370 seconds to approximately 80 seconds. According to the data in Table 1, the improvements led to reduced misalignment, more consistent bonding, and enhanced production efficiency. The integration with existing automation infrastructure remained intact, including PID-controlled heaters and a machine vision system. Operators reported easier alignment, reduced thermal distortion, and more predictable process control, supporting the viability

of this design in a regulated manufacturing environment.

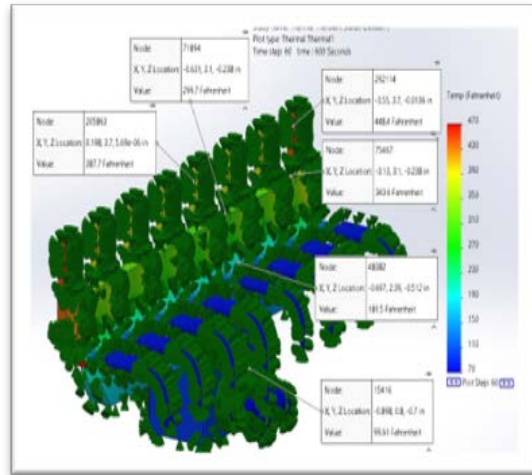


Figure 1
Original Transient State Study

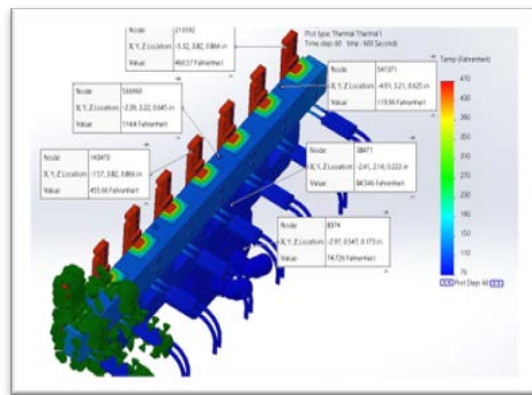


Figure 2
New Design Transient State Study

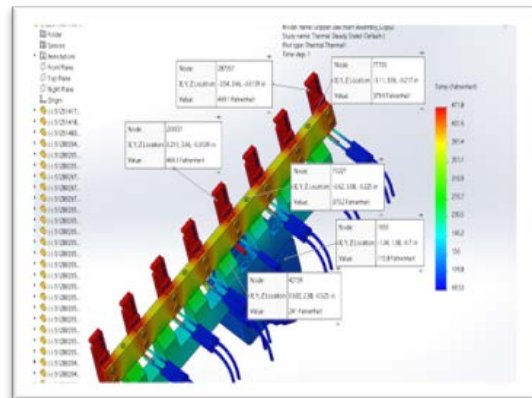


Figure 3
Original Design Steady State Study

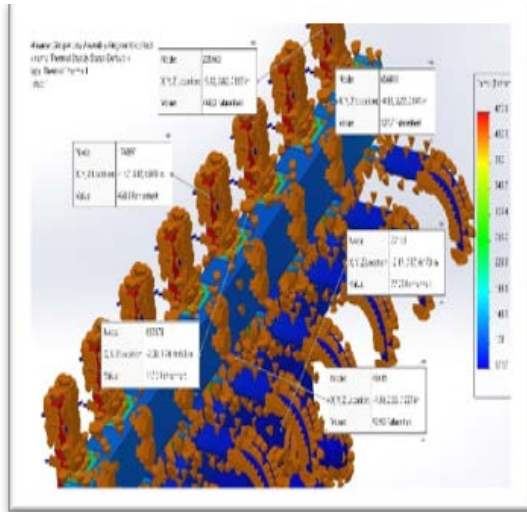


Figure 4
New Design Steady State Study

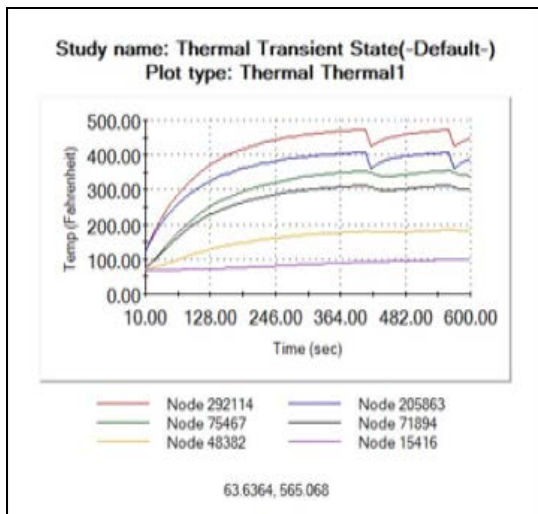


Figure 5
Transient Study Original Design

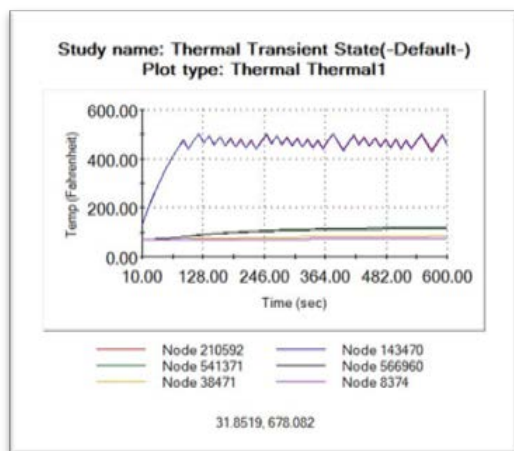


Figure 6
Transient Study New Design

Table 1
Original vs New Design Performance

Metric	Original System	Redesigned System	Improvement
Copper Insert Temp (Transient)	387.7°F to 448.4°F	455.7°F to 460.6°F	~5°F variation vs. ~60°F spread
INVAR Bar Temp (Transient)	299.7°F to 340.6°F	114.4°F to 119.9°F	~65% reduction
Holding Mount Temp (Transient)	181.5°F	84.5°F	~53% reduction
Copper Insert Temp (Steady)	469.1°F to 469.14°F	468.3°F (uniform)	Comparable, but more uniform
INVAR Bar Temp (Steady)	373.2°F to 379.9°F	117.5°F to 127.7°F	~66% reduction
Mounting Block Temp (Steady)	241°F	92°F	~62% reduction
Stabilization Time	~370 seconds	~80 seconds	~79% faster heat-up time
Thermal Misalignment	Frequent	None observed (mechanically stable)	Improved alignment control
Assembly Ease	Moderate	Easy	Better modularity and usability

CONCLUSION

The redesign of the thermal bonding system for pacemakers effectively addresses the challenges of thermal inconsistency and mechanical misalignment. By integrating Celazole insulation and optimizing the heat transfer pathway, the system achieved superior thermal stability and faster cycle times. Finite Element Analysis (FEA) validated the performance gains in both transient and steady-state conditions, demonstrating reduced heat propagation and improved bond quality. The solution proved compatible with existing automation, maintaining process control integrity and inspection accuracy. This work establishes a scalable, efficient, and robust platform for high-precision medical device manufacturing and can serve as a reference for similar thermally driven assembly processes.

RECOMMENDATIONS AND FUTURE WORK

While the redesigned thermal bonding system demonstrated marked improvements in heat distribution and cycle efficiency, additional enhancements are recommended to further optimize its performance:

- **Experimental Validation:** Mechanical bond strength testing under various production conditions is advised to validate the durability and quality of the bonded joints.
- **Advanced Thermal Simulation:** Future Finite Element models should include surface-to-ambient radiation effects and airflow-dependent convection coefficients to simulate real-world thermal environments more accurately.
- **Material Innovation:** Investigate alternative insulating materials with better machinability or thermal resistance and evaluate geometric optimizations of the Celazole insert for further heat confinement.
- **Design for Manufacturability (DFM):** A formal DFM review is suggested to prepare the system for broader implementation, ensuring cost-effective scaling and robust assembly protocols.
- **Broader Applications:** The modularity and thermal precision of this system make it a candidate for similar applications in catheters, micro-sensors, and other precision medical devices that require tightly controlled thermal bonding.

SIMULATIONS CONSIDERATIONS

To ensure manageable simulation complexity and computation time, certain assumptions were made during the Finite Element Analysis (FEA):

- **Convection Modeling:** A constant convection heat transfer coefficient of $38 \text{ W/m}^2\text{-K}$ was applied to all external surfaces. While this approximates enhanced natural or low-level forced convection, real-life variations due to

airflow or surface orientation were not considered.

- **Neglect of Thermal Radiation:** Radiative heat transfer, especially relevant at elevated temperatures ($>300^\circ\text{F}$), was excluded to reduce simulation complexity. Including radiation could affect temperature distributions, particularly near high-temperature copper inserts.
- **Material Properties Assumed Constant:** Thermal conductivity, heat capacity, and expansion coefficients were considered temperature independent. This simplification may affect the accuracy of high-temperature predictions, especially for polymers like polyurethane.
- **Mesh Granularity:** A relatively coarse mesh was used for initial iterations to reduce solver time. While convergence was verified for critical regions (insert-polymer interface), future high-fidelity simulations could use localized mesh refinement.

Despite these simplifications, the simulations were sufficient to capture critical thermal trends and guide effective redesign decisions. Future work could involve experimental thermal imaging or embedded sensor validation against benchmarks and improving the accuracy of the numerical model.

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